For both parts, we are given:

$$\boldsymbol{\omega} = 0.5 \mathbf{k} \text{ rad/s}, \quad \boldsymbol{\alpha} = 0.2 \mathbf{k} \text{ rad/s}^2, \quad \mathbf{v}_O = \mathbf{0}, \quad \mathbf{a}_O = \mathbf{0}.$$

(a) For the straight path and point D:

$$\mathbf{v}_{g/\mathcal{B}} = 0.75 \mathbf{j} \text{ m/s}, \quad \mathbf{a}_{g/\mathcal{B}} = \mathbf{0}, \quad \mathbf{r}_{D/O} = 1 \mathbf{i} \text{ m}.$$

The absolute velocity is therefore:

$$\mathbf{v}_g = \mathbf{v}_O + \boldsymbol{\omega} \times \mathbf{r}_{D/O} + \mathbf{v}_{g/B}$$
  
=  $\mathbf{0} + (0.5)(1)\mathbf{j} \text{ m/s} + 0.75\mathbf{j} \text{ m/s}$   
=  $1.25\mathbf{j} \text{ m/s}.$ 

and the absolute acceleration is:

$$\mathbf{a}_{g} = \mathbf{a}_{O} + \boldsymbol{\alpha} \times \mathbf{r}_{D/O} + \boldsymbol{\omega} \times (\boldsymbol{\omega} \times \mathbf{r}_{D/O}) + \mathbf{a}_{g/\mathcal{B}} + 2\boldsymbol{\omega} \times \mathbf{v}_{g/\mathcal{B}} 
= \mathbf{0} + (0.2)(1)\mathbf{j} \text{ m/s}^{2} - (0.5)(0.5)(1)\mathbf{i} \text{ m/s}^{2} + \mathbf{0} - 2(0.5)(0.75)\mathbf{i} \text{ m/s}^{2} 
= (-1.0\mathbf{i} + 0.2\mathbf{j}) \text{ m/s}^{2}.$$

(b) For the circular path and point B:

$$\mathbf{v}_{g/\mathcal{B}} = 0.75 \mathbf{j} \text{ m/s}, \quad \mathbf{a}_{g/\mathcal{B}} = -v_{g/\mathcal{B}}^2 / r_{B/O} \mathbf{i} = -0.1875 \mathbf{i} \text{ m/s}^2, \quad \mathbf{r}_{B/O} = 3\mathbf{i} \text{ m}.$$

The absolute velocity is now:

$$\mathbf{v}_g = \mathbf{v}_O + \boldsymbol{\omega} \times \mathbf{r}_{B/O} + \mathbf{v}_{g/B}$$
  
=  $\mathbf{0} + (0.5)(3)\mathbf{j} \text{ m/s} + 0.75\mathbf{j} \text{ m/s}$   
=  $2.25\mathbf{j} \text{ m/s}.$ 

and the absolute acceleration is:

$$\mathbf{a}_{g} = \mathbf{a}_{O} + \boldsymbol{\alpha} \times \mathbf{r}_{B/O} + \boldsymbol{\omega} \times (\boldsymbol{\omega} \times \mathbf{r}_{B/O}) + \mathbf{a}_{g/\mathcal{B}} + 2\boldsymbol{\omega} \times \mathbf{v}_{g/\mathcal{B}} = \mathbf{0} + (0.2)(3)\mathbf{j} \text{ m/s}^{2} - (0.5)(0.5)(3)\mathbf{i} \text{ m/s}^{2} - 0.1875\mathbf{i} \text{ m/s}^{2} - 2(0.5)(0.75)\mathbf{i} \text{ m/s}^{2} = (-1.6875\mathbf{i} + 0.6\mathbf{j}) \text{ m/s}^{2}.$$

2. The 15-lb disk rests on the 5-lb plate. A cord is wrapped around the periphery of the disk and attached to the wall at B. If a torque  $M = 40 \text{ lb} \cdot \text{ft}$  is applied to the disk, determine the angular acceleration of the disk and the time needed for the end C of the plate to travel 3 ft and strike the wall. The disk does not slip on the plate and the surface at D is smooth. Neglect the mass of the cord. (18 points total).

The FBD and MAD of the disk and the plate can be drawn as:



Summing the moments around A for the disk, and the horizontal forces for the plate, we obtain:

$$\sum M_A = M - F \cdot 2R = \bar{I}\alpha + m_1\bar{a}_1R,$$
$$\sum F_x = F = m_2\bar{a}_2.$$

Because of the cord, the disk undergoes instantaneous angular motion about A, and therefore  $\bar{a}_1 = \alpha R$ . Since there is no slipping on the plate, we also conclude that  $\bar{a}_2 = \alpha \cdot 2R$ . Substituting these kinematic relations into the FMA equations above, we obtain two equations for two unknowns F and  $\alpha$ :

$$F = m_2 \alpha \cdot 2R,$$
  

$$M - m_2 \alpha \cdot 4R^2 = \frac{1}{2}m_1 R^2 \alpha + m_1 \alpha \cdot R^2,$$
  

$$M = (4m_2 + 1.5m_1)R^2 \alpha.$$

The angular acceleration of the disk can be now computed as:

$$\alpha = \frac{M}{(4m_2 + 1.5m_1)R^2},$$
  
=  $\frac{40 \cdot 32.2}{(4 \cdot 4 + 1.5 \cdot 15)1.25^2}$   
= 19.396 rad/s<sup>2</sup>.

The linear acceleration of the plate is therefore constant at:

$$\bar{a}_2 = \alpha \cdot 2R = 19.396 \cdot 2 \cdot 1.25 = 48.489 \text{ ft/s}^2.$$

Under constant acceleration and starting from rest, the time needed to travel the 3 ft distance is:

$$t = \sqrt{\frac{2s}{\bar{a}_2}} = 0.3518 \text{ s}$$

3. The collar *B* has a mass of 3 kg and may slide freely on rod *OA*, which in turn may rotate freely in the horizontal plane. The assembly is rotating with an angular velocity  $\omega = 1.8$  rad/s when a spring located between *A* and *B* is released, projecting the collar along the rod with an initial relative speed  $v_r = 1.5$  m/s. Knowing that the moment of inertia about *O* of the rod and spring is 0.35 kg  $\cdot$  m<sup>2</sup>, determine (a) the minimum distance between the collar and point *O* in the ensuing motion, (b) the corresponding angular velocity of the assembly. (18 points total).

Just after the collar is released (state 1), the velocity of the collar is due to the angular motion of the assembly and the radial motion of the collar along the rod. At the minimum distance from O (state 2), the collar has stopped moving along the rod and its velocity is only due to the angular motion of the assembly. The momentum diagrams for these two states are shown below, with unknowns  $r_2$  and  $\omega_2$  to be determined.



Here,  $(v_1)_r = 1.5$  m/s and  $(v_1)_{\theta} = 0.5 \cdot 1.8 = 0.9$  m/s, and  $(v_2)_r = 0$  m/s and  $(v_2)_{\theta} = r_2 \omega_2$ .

Noticing that the collar is free-sliding, and that the normal reactions at the collar do not do any net work on the assembly, we conclude that the kinetic energy of the assembly is conserved between states 1 and 2. Noticing also that there is no moment of external forces about the axis of rotation, we conclude that the angular momentum about that axis is also conserved. The kinetic energy  $T_1$  and the angular momentum  $h_1$  can be computed as:

$$T_{1} = \frac{1}{2}I\omega_{1}^{2} + \frac{1}{2}mv_{1}^{2}$$
  
=  $\frac{1}{2} \cdot 0.35 \cdot 1.8^{2} + \frac{1}{2} \cdot 3 \cdot (1.5^{2} + 0.9^{2})$   
=  $0.567 + 4.59 = 5.157$  Nm,  
 $h_{1} = I\omega_{1} + m(v_{1})_{\theta}r_{1}$   
=  $0.35 \cdot 1.8 + 3 \cdot 0.9 \cdot 0.5$   
=  $0.63 + 1.35 = 1.98$  Nms.

$$T_{2} = \frac{1}{2}I\omega_{2}^{2} + \frac{1}{2}m(v_{2})_{\theta}^{2}$$
  

$$= \frac{1}{2} \cdot 0.35 \cdot \omega_{2}^{2} + \frac{1}{2} \cdot 3 \cdot \omega_{2}^{2}r_{2}^{2}$$
  

$$= (0.175 + 1.5r_{2}^{2})\omega_{2}^{2} = T_{1},$$
  

$$h_{2} = I\omega_{2} + m(v_{2})_{\theta}r_{2}$$
  

$$= 0.35 \cdot \omega_{2} + 3 \cdot \omega_{2}r_{2}^{2}$$
  

$$= (0.35 + 3r_{2}^{2})\omega_{2} = h_{1}.$$

Substituting  $\omega_2 = h_1/(0.35 + 3r_2^2)$  into the first equation above yields:

$$r_2^2 = \frac{\frac{1}{2}h_1^2/T_1 - 0.35}{3},$$

and  $r_2 = 100.17$  mm and  $\omega_2 = 5.209$  rad/s.