

## Distributed Elastic Support Data for the Human Palm

Recent data has been published on the human palm as an elastic foundation. The foundation modulus should be reported with the units of  $(\text{N}/\text{m}^2)/\text{m}$ . The reference paper used an indenter having a diameter of 2 mm and an area of  $3.142 \text{ mm}^2$ . The tabulated point stiffnesses  $(\text{N}/\text{mm})$  need to be divided by the indenter area to get the distributed foundation modulus,  $\text{N}/\text{mm}^3$ .

For example, the distal medial palm average point stiffness of 2.34  $\text{N}/\text{mm}$  should have been reported as  $k = 0.745 \text{ N}/\text{mm}^3 = 7.45\text{e}8 (\text{N}/\text{m}^2)/\text{m}$ .

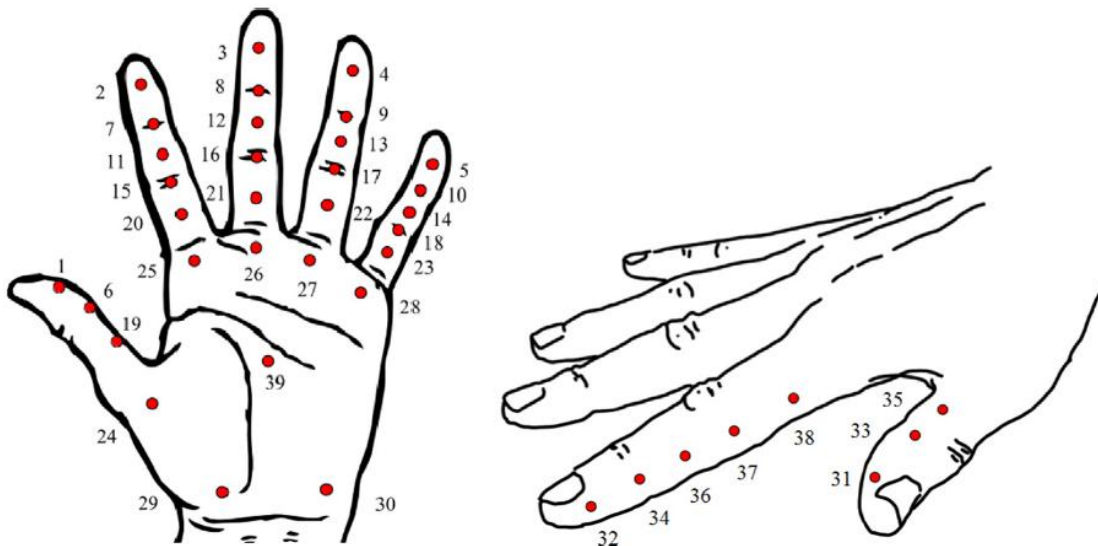
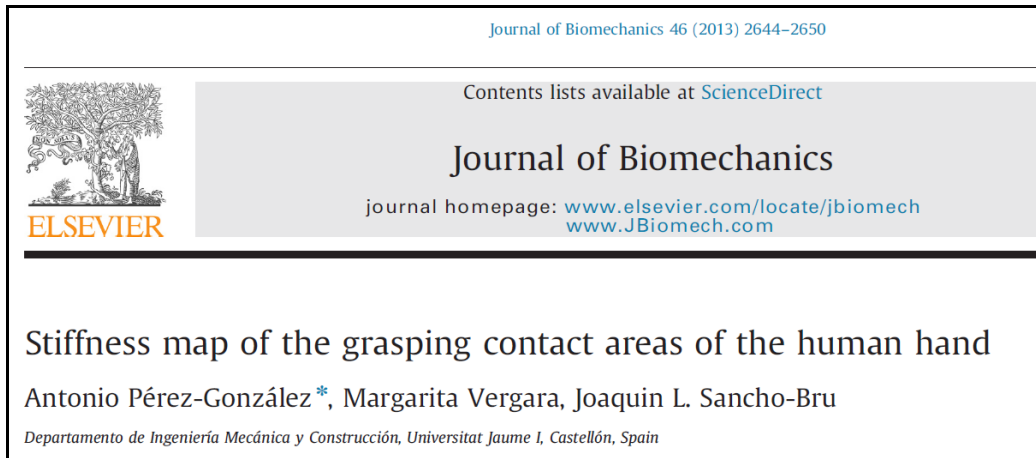


Fig. 1. Location of the points for measurement on the hand.

**Table 3**  
Classification of points in regions with similar mean stiffness.

| Region  | Nick      | Points         |
|---|-----------|----------------|
| Distal phalange of thumb                              | DP_T      | 1              |
| Distal phalanges of fingers                           | DP_F      | 2,3,4,5        |
| Distal interphalangeal joints                         | Joint_DIP | 7,8,9,10       |
| Proximal interphalangeal joints                       | Joint_PIP | 6,15,16,17,18  |
| Intermediate phalanges                                | MP        | 11,12,13,14    |
| Proximal phalanges                                    | PP        | 19,20,21,22,23 |
| Medial and proximal palm                              | M&P_Palm  | 24,29,30,39    |
| Distal palm middle finger                             | D_Palm_M  | 26             |
| Rest of distal palm                                   | D_Palm    | 25,27,28       |
| Lateral side of distal phalange of thumb              | Lat_DP_T  | 31             |
| Lateral side of intermediate phalange of index        | Lat_MP_I  | 36             |
| Lateral side of joints of thumb and index             | Lat_Joint | 33,34,37       |
| Rest of lateral side of proximal and distal phalanges | Lat_P&D   | 32,35,38       |

**Table 4**  
Mean (SD) of the stiffness (N/mm) by region and force interval (20 subjects).

|           | Force interval |            |            |            |            |            |
|-----------|----------------|------------|------------|------------|------------|------------|
|           | s01            | s12        | s23        | s34        | s45        | s56        |
| DP_T      | 0.23(0.04)     | 1.37(0.44) | 2.45(0.73) | 3.25(1.00) | 4.20(1.37) | 4.67(1.81) |
| DP_F      | 0.27(0.04)     | 1.86(0.63) | 3.61(1.27) | 4.72(1.41) | 6.12(1.61) | 6.88(1.94) |
| Joint_DIP | 0.50(0.13)     | 2.38(1.12) | 3.96(1.55) | 4.83(1.33) | 6.01(1.79) | 6.64(2.14) |
| Joint_PIP | 0.80(0.30)     | 2.76(1.13) | 3.56(1.45) | 3.66(1.44) | 4.00(1.69) | 4.16(1.74) |
| MP        | 0.35(0.09)     | 1.48(0.57) | 2.60(1.06) | 3.45(1.15) | 4.41(1.53) | 4.64(1.63) |
| PP        | 0.28(0.07)     | 1.18(0.43) | 1.95(0.90) | 2.33(0.95) | 2.88(1.30) | 2.95(1.31) |
| M&P_Palm  | 0.24(0.09)     | 0.55(0.18) | 0.74(0.26) | 0.83(0.30) | 1.03(0.41) | 1.10(0.55) |
| D_Palm_M  | 0.36(0.12)     | 1.71(0.86) | 2.38(0.94) | 2.16(1.20) | 2.47(1.45) | 1.88(0.96) |
| D_Palm    | 0.30(0.12)     | 1.25(0.60) | 1.78(0.91) | 1.95(1.16) | 2.03(0.98) | 1.87(0.90) |
| Lat_DP_T  | 0.44(0.12)     | 1.45(0.59) | 1.98(0.75) | 2.17(0.61) | 2.75(0.79) | 2.83(0.97) |
| Lat_MP_I  | 0.93(0.42)     | 3.10(1.54) | 3.73(1.31) | 4.02(1.19) | 4.98(1.67) | 4.62(1.70) |
| Lat_Joint | 0.92(0.28)     | 4.03(1.57) | 5.52(2.15) | 5.40(2.16) | 6.12(2.28) | 5.76(2.07) |
| Lat_P&D   | 0.50(0.18)     | 2.67(1.47) | 3.06(1.24) | 3.19(1.31) | 3.43(1.39) | 3.51(1.74) |

To validate the SW elastic foundation model a part was created with a 2 mm diameter and a length of 12 mm (to reduce large deflection problems). It was made of alloy steel. It was considered as an indenter pressing on the palm. The top end was loaded axially with 2.34 N. The bottom end was assumed to be the palm and was assigned an elastic support modulus of  $7.45 \times 10^8 \text{ N/mm}^3$ . This part should mainly translate vertically ( $y$ -direction) exactly 1 mm if the part were perfectly rigid, but will be a little less than that due to deformation of the steel.

The cylindrical surface was restrained in the radial and circumferential directions to prevent rigid body motion (but allow  $y$ -direction motion). The computed  $y$ -displacement using the iterative solver was 0.996 mm which matches the expected result (the direct solver failed).

### Connectors ?

✓
✗
- [ ]

Type Split

**Message**

For accurate results, the movement of the selected faces should be small relative to the thickness of the support.

**Type**

[ ] Elastic Support

[ ] Face<1>

**Stiffness**

[ ] SI

Distributed  
 Total

[ ] 745000000 (N/m)/m<sup>2</sup>

[ ] 0 (N/m)/m<sup>2</sup>

**Symbol Settings**

|  |           |
|--|-----------|
| Normal ((N/m)/m <sup>2</sup> ):                | 745000000 |
| Shear ((N/m)/m <sup>2</sup> ):                 | 0         |
| Compression preload force (N/m <sup>2</sup> ): | 0         |

